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Fuel Assembly Bow DNBR Penalty for VVER-1000 reactors

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Outline

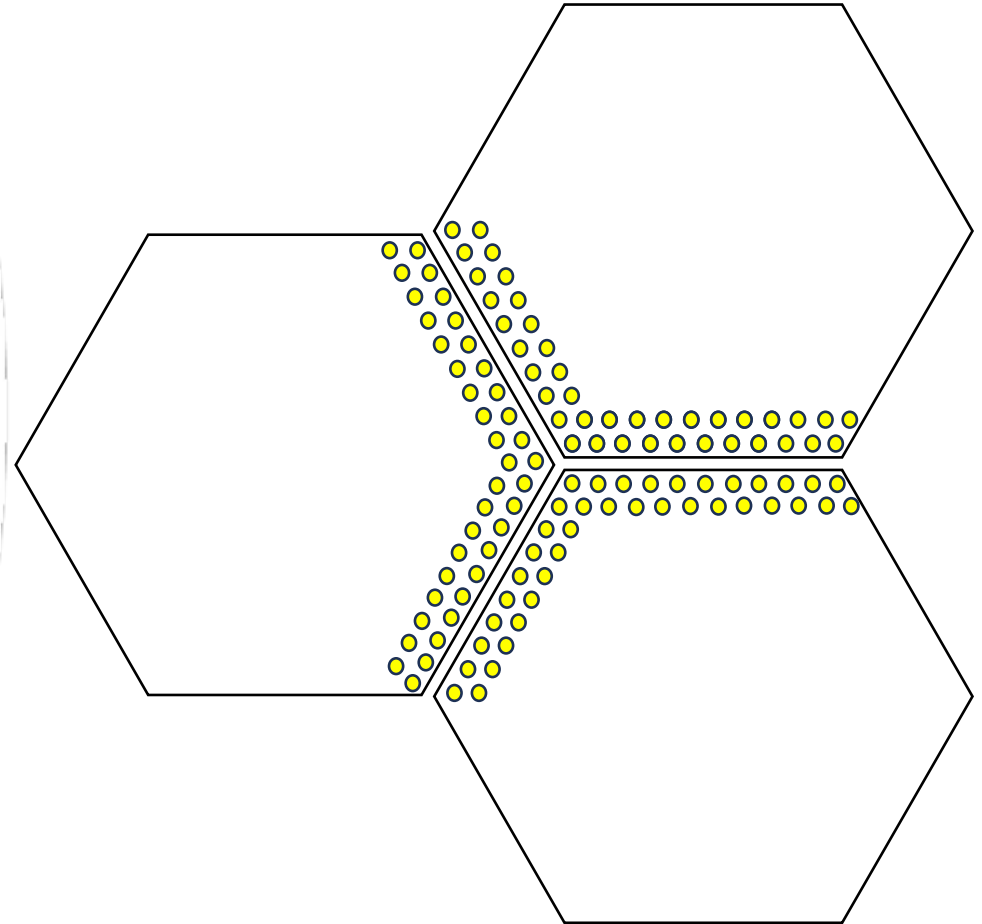
- Core modelling with increased inter-assembly gap for TH analysis
- Methodology
- Design Limit DNBR Analysis
- Verification of DL DNBR for increased gap conditions
- Results

Full Core Model with increased inter-assembly gap



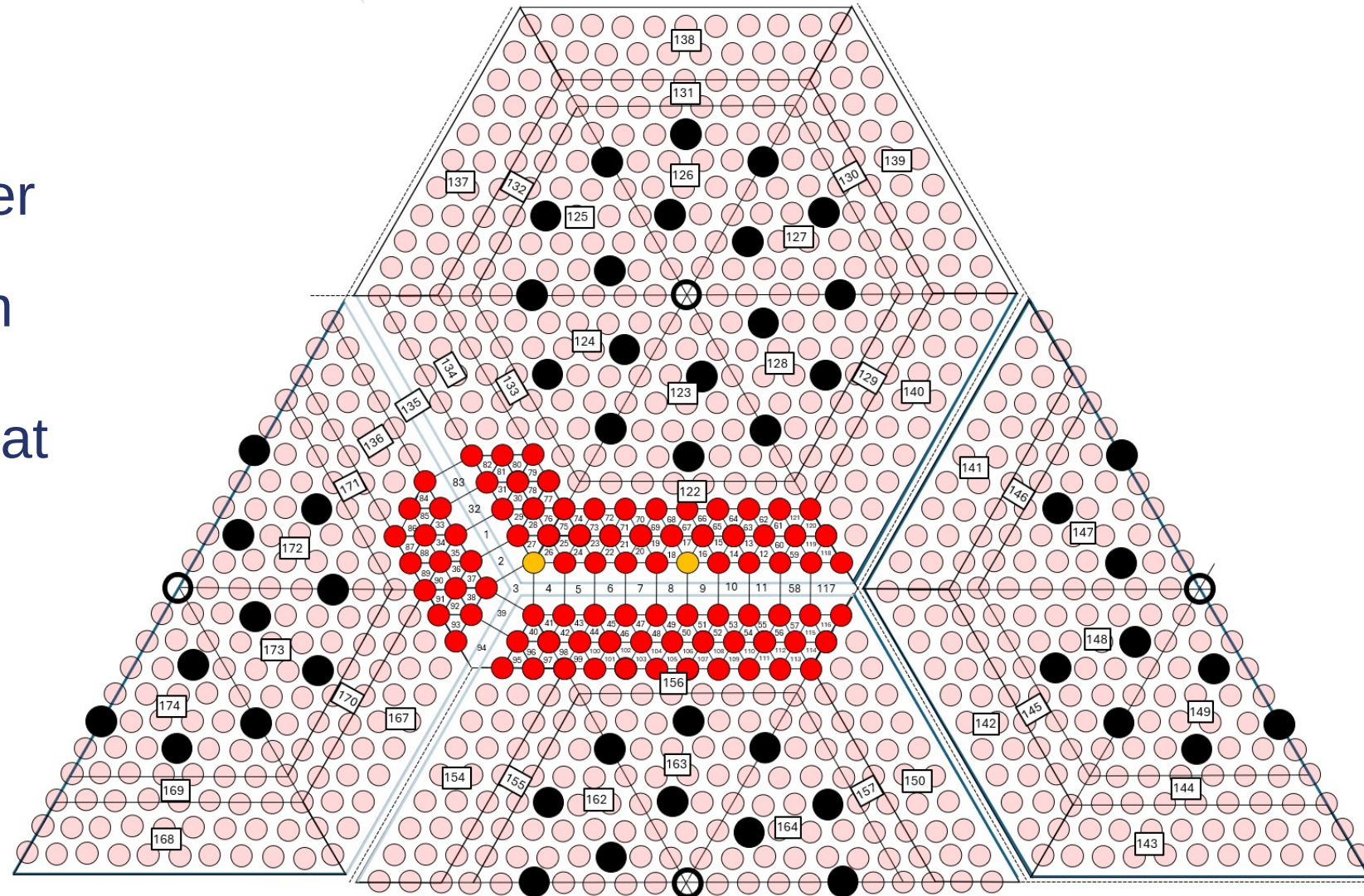
Increase of the inter-assembly gap

- Increased assembly-to-assembly gap impacts to local power and integral rod power due to over-moderation
- Impact on DNB is evaluated for hot channels located at periphery of FA (side and corner)

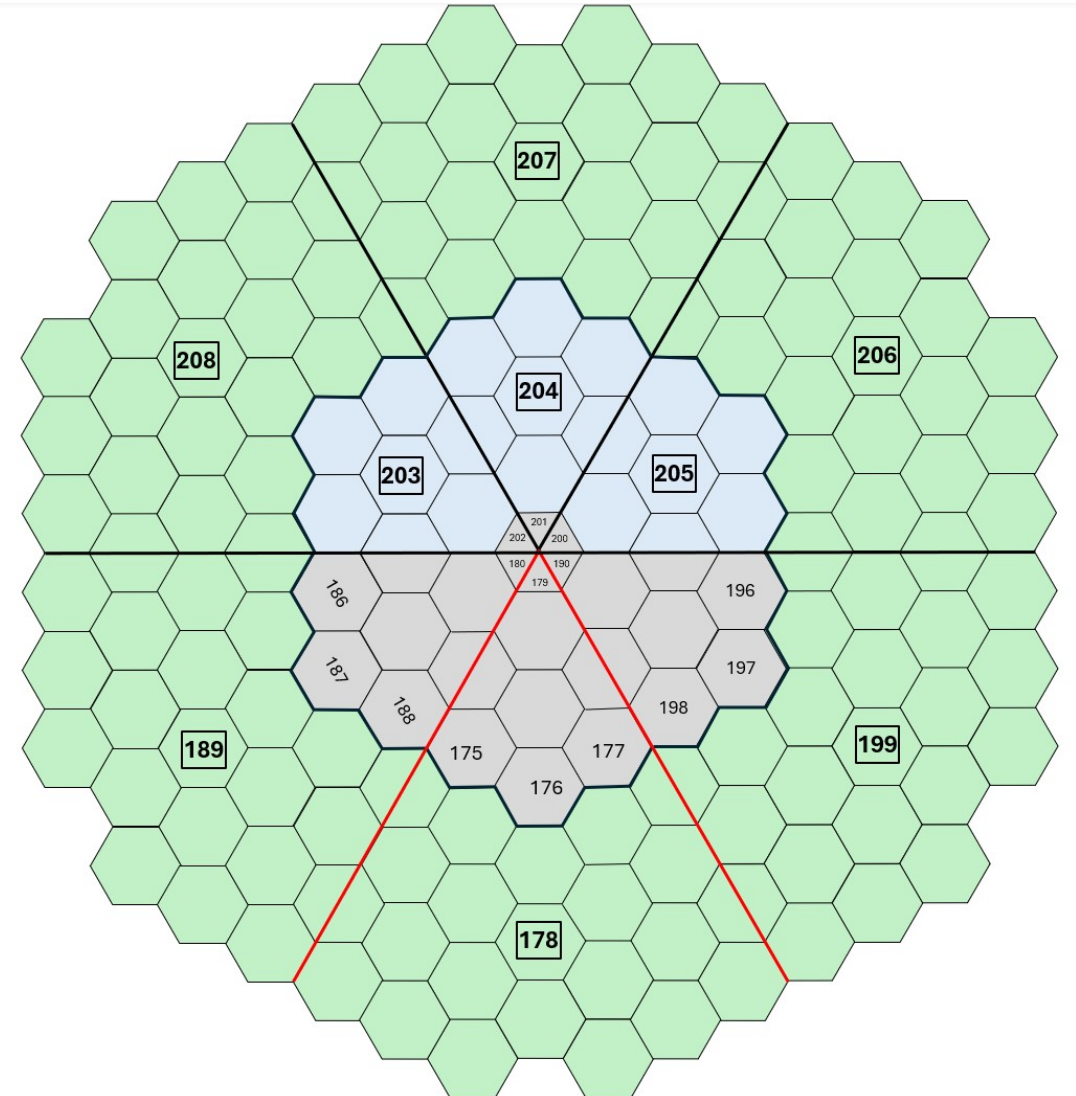
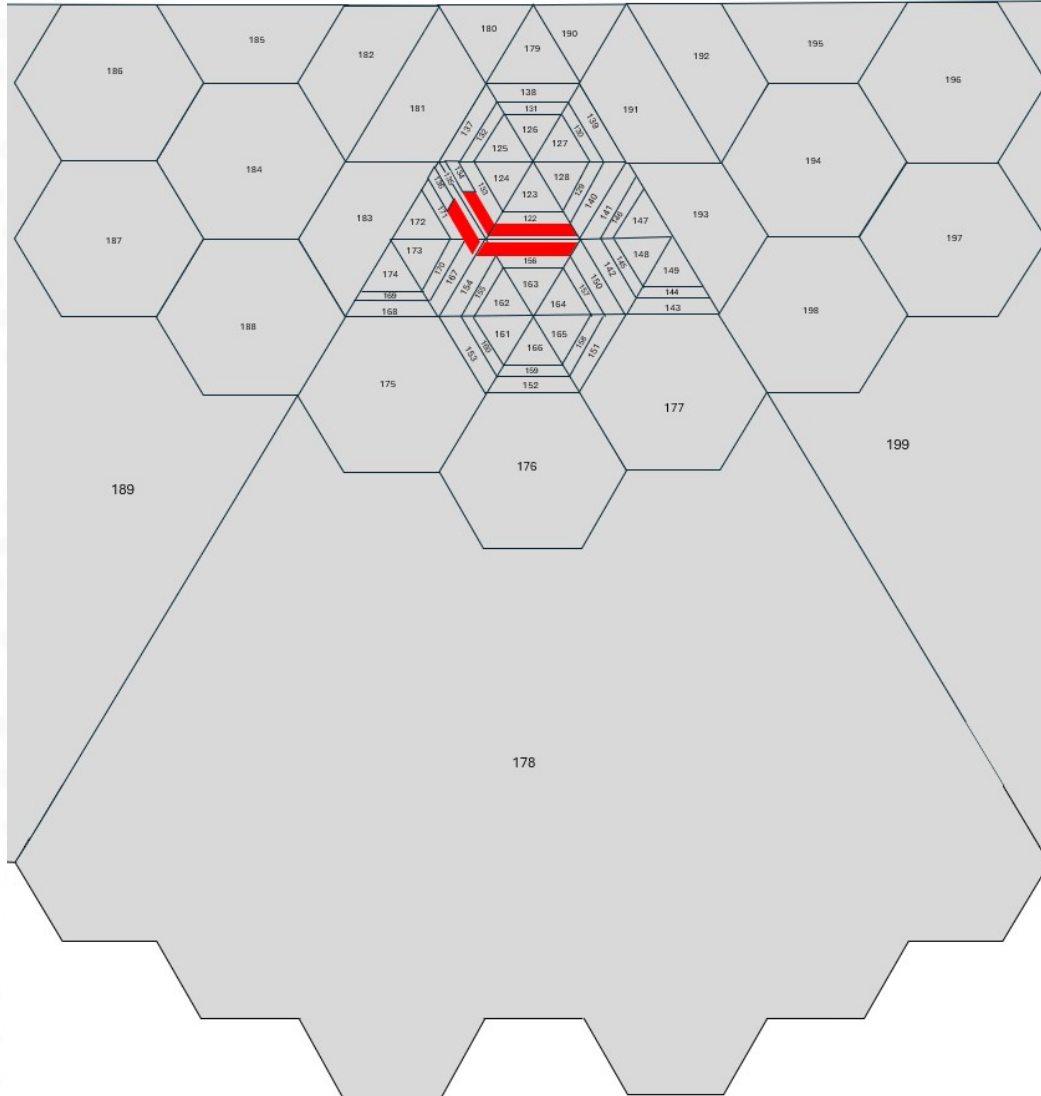


Full Core VVER-1000 Model: 208-channels VIPRE Model

- A VVER-1000 reactor core is modeled in a relatively small number of channels without losing any accuracy in DNBR predictions
- Hot channels located at periphery of FA and their adjacent region are modeled in detail, while the rest of the core is modeled as lumped channels



Full Core VVER-1000 Model: 208-channels VIPRE Model



Methodology

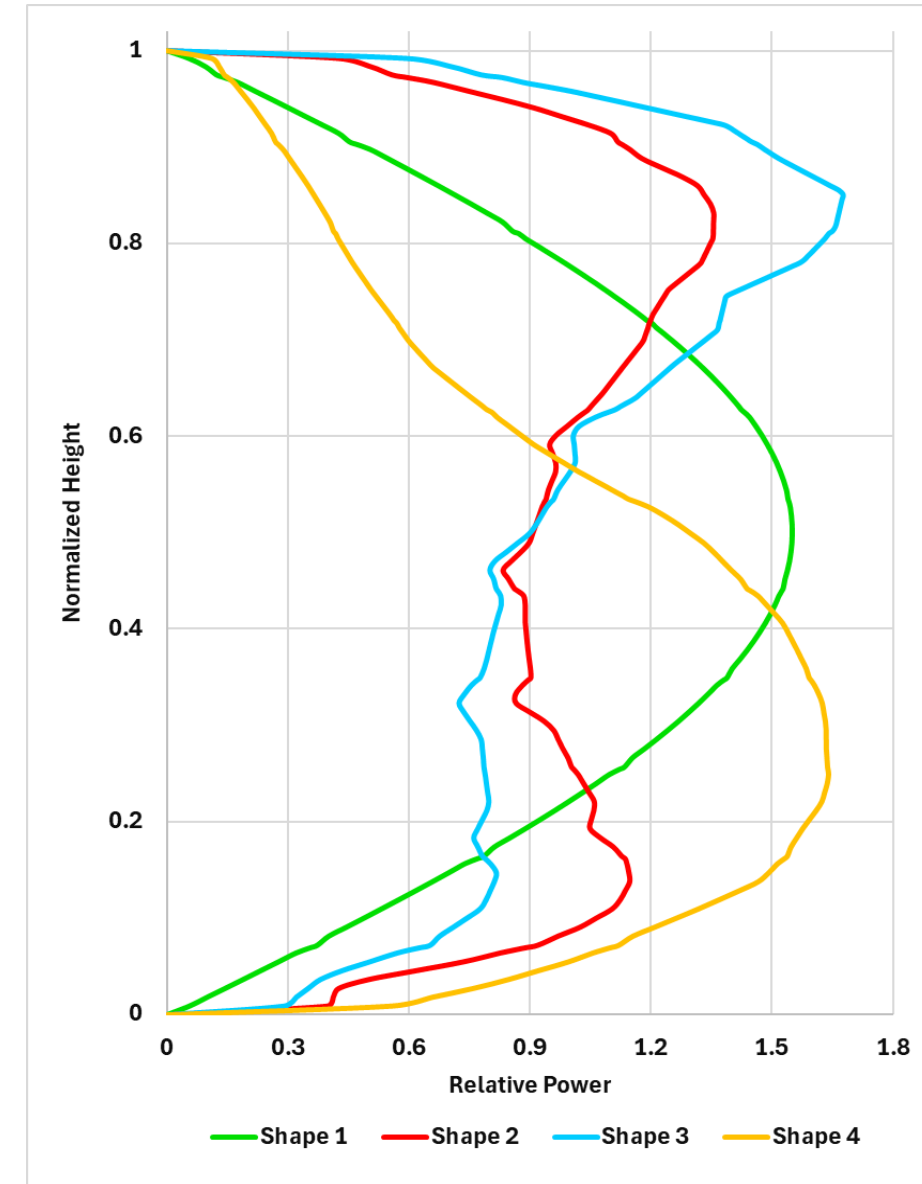


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Methodology: Statistical DNBR Analysis

Reactor Uncertainties
+
CHF corr. Uncertainty

- **DL DNBR** for side and corner channels.
- CHF correlation is used for grids with and without vanes
- 10 Reactor Limiting Operational Conditions.
- Power, Pressure, Inlet flow, Inlet Temperature.
- 4 different axial power shapes.
- $F_{\Delta H}^{Design}$
- Hot FAs power $F_{\Delta H}^{Design} / 1.04$ which is the highest FA power.
- Gap_{nominal} = 2mm



Methodology: Increase of Inter-assembly gap and rods power

- The methodology is applied to all 10 cases.
- The maximum gap has been increased at step of 1mm.
- For each value of max gap, the axial gap distribution has been evaluated as follow

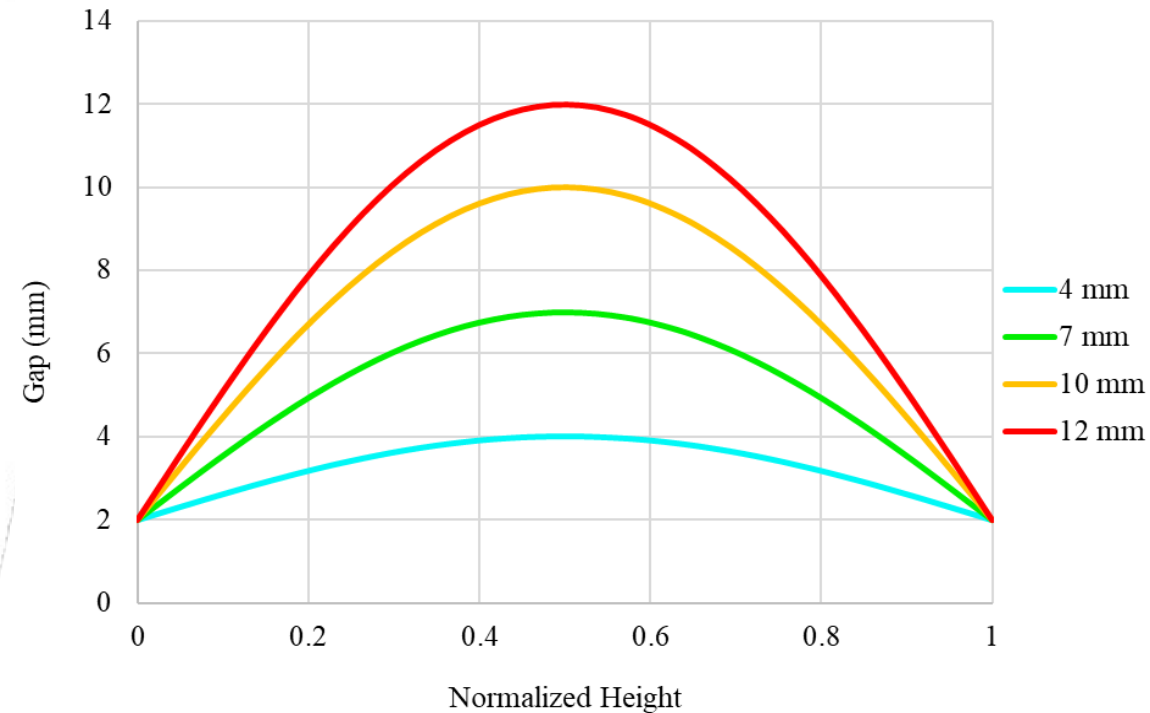
- $gap(z) = gap_{nominal} + \Delta gap_{max} \sin\left(\frac{\pi z}{H}\right)$

- Where:

$$gap_{nominal} = 2 \text{ mm}$$

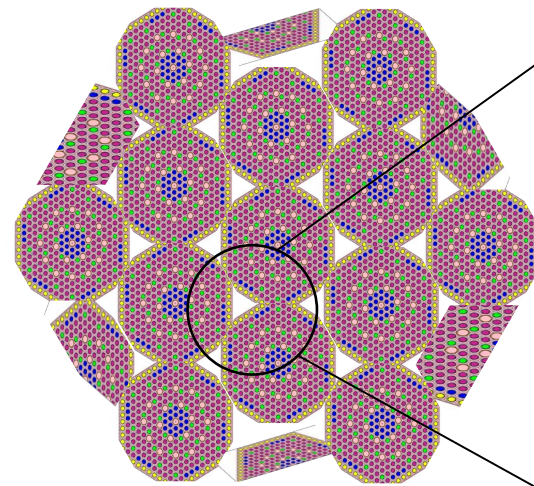
$$\Delta gap_{max} = gap_{max,j} - gap_{nominal}$$

- The gap distribution is going to impact the hydraulic parameters of peripheral cells which have been changed consequently.

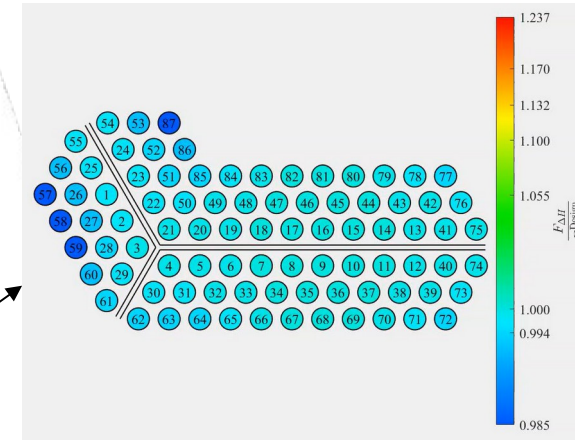


Methodology: Increase of Inter-assembly gap and rods power

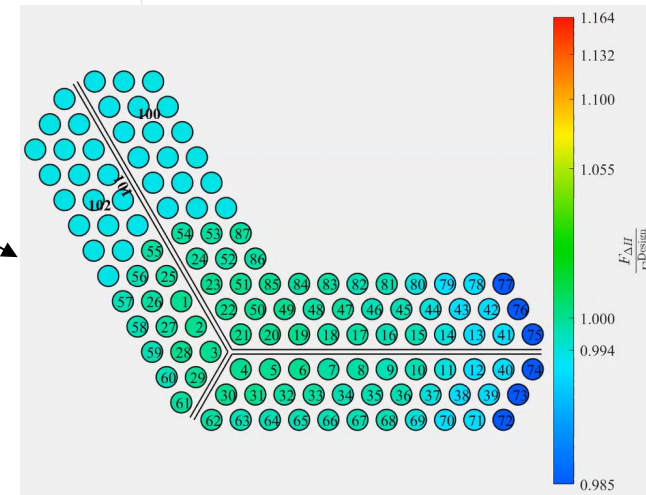
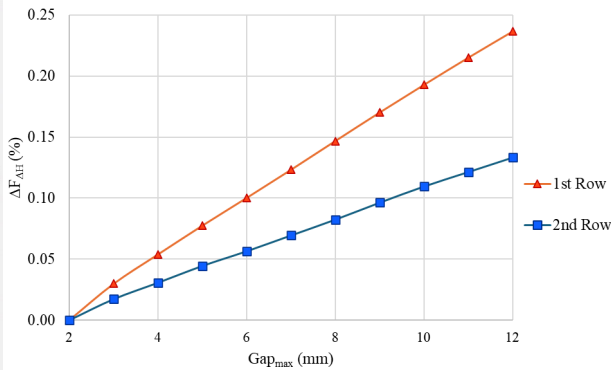
- Mini-Core with 19 FAs with highest reactivity
- Power rods is a function of inter-assembly gap
- MCNP: Monte-Carlo code



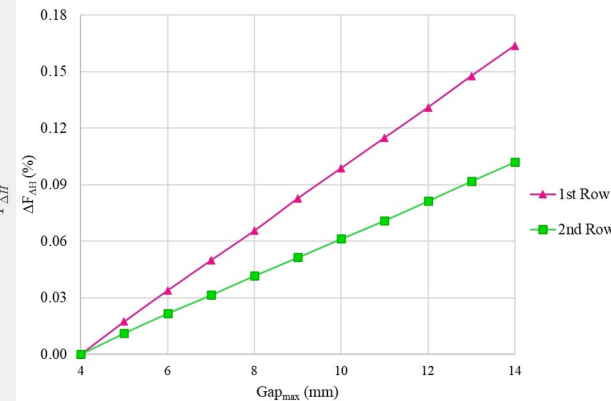
- Enrichment-1
- Enrichment-2
- Enrichment-3
- Gad-rods



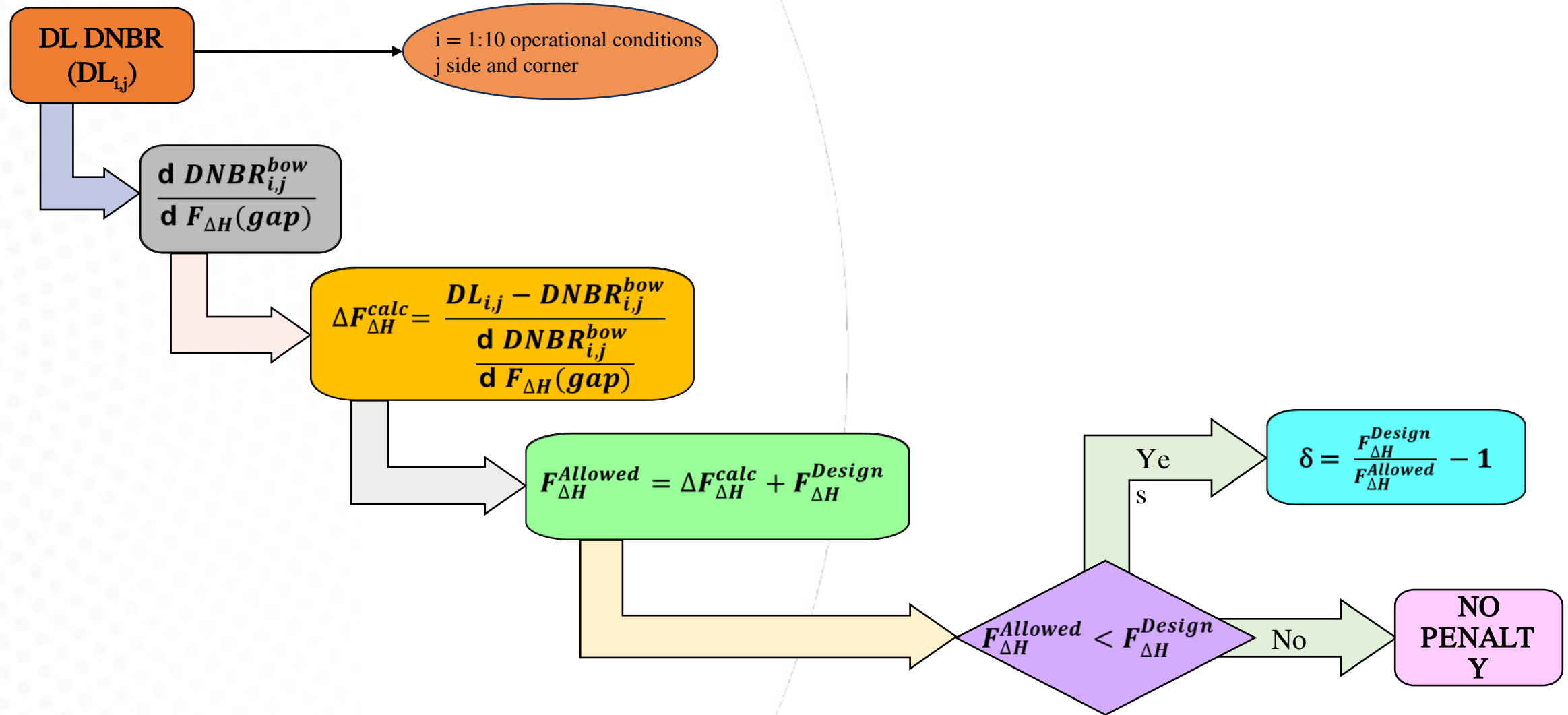
1-sided gap – distance along the normal between opposite faces of adjacent FA



2-sided gap – sum of two distances along the normal between opposite faces of two adjacent FA



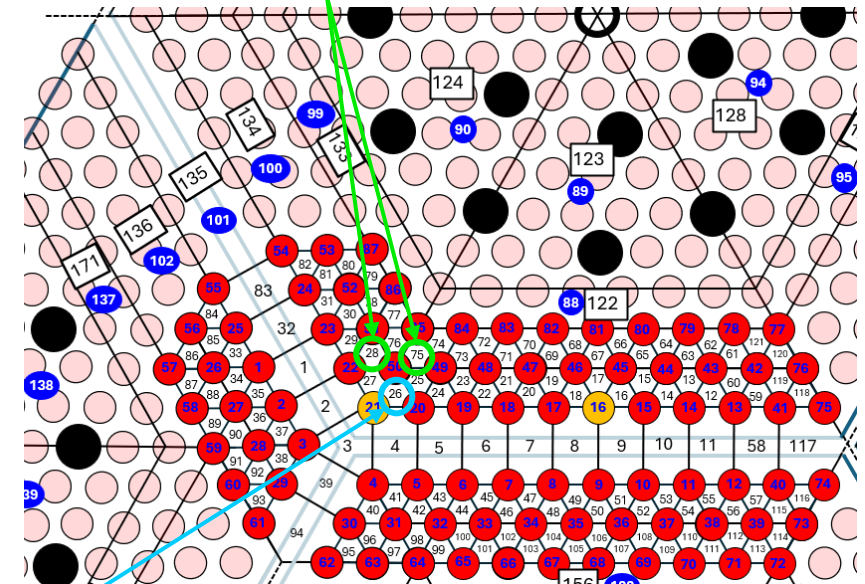
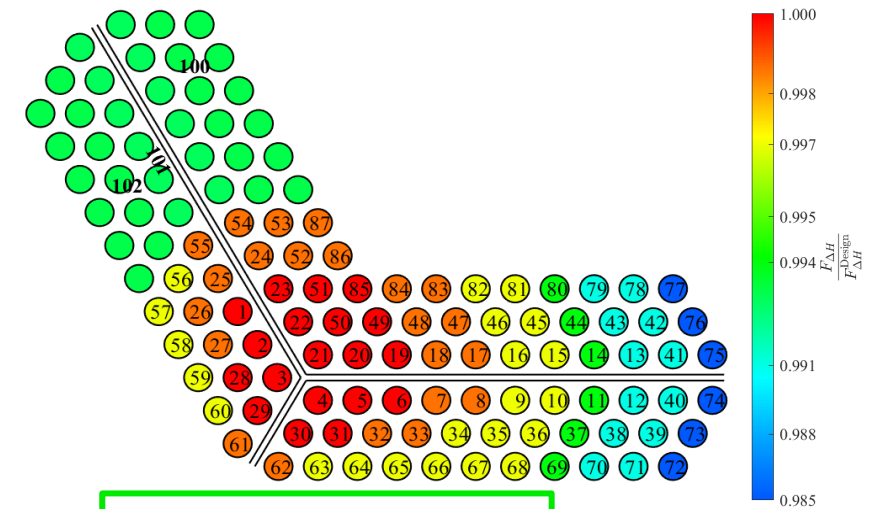
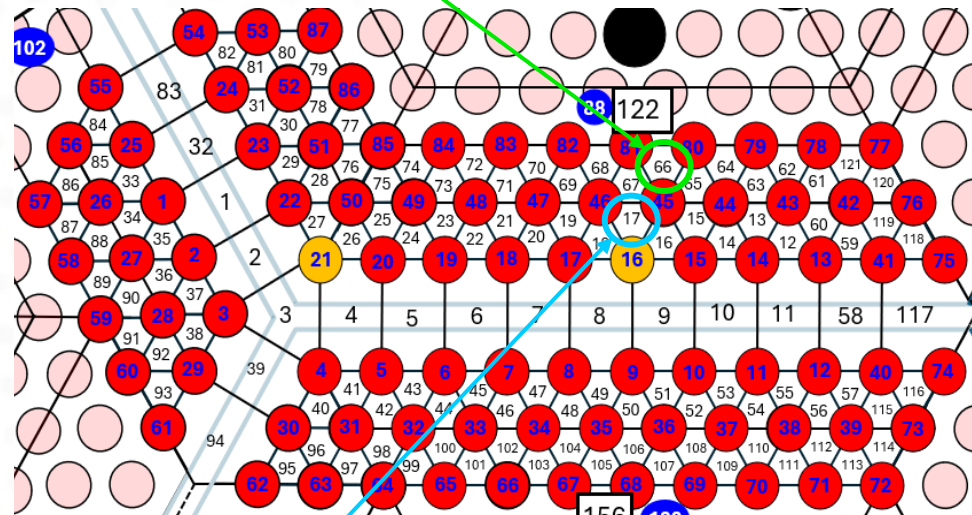
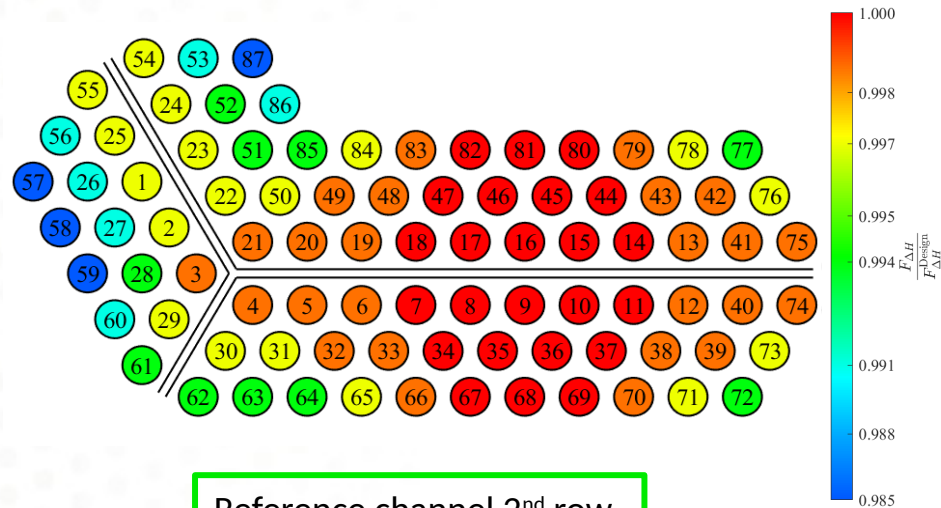
Methodology: $F_{\Delta H}$ penalty (δ)



Verification of DL DNBR for increased gap conditions

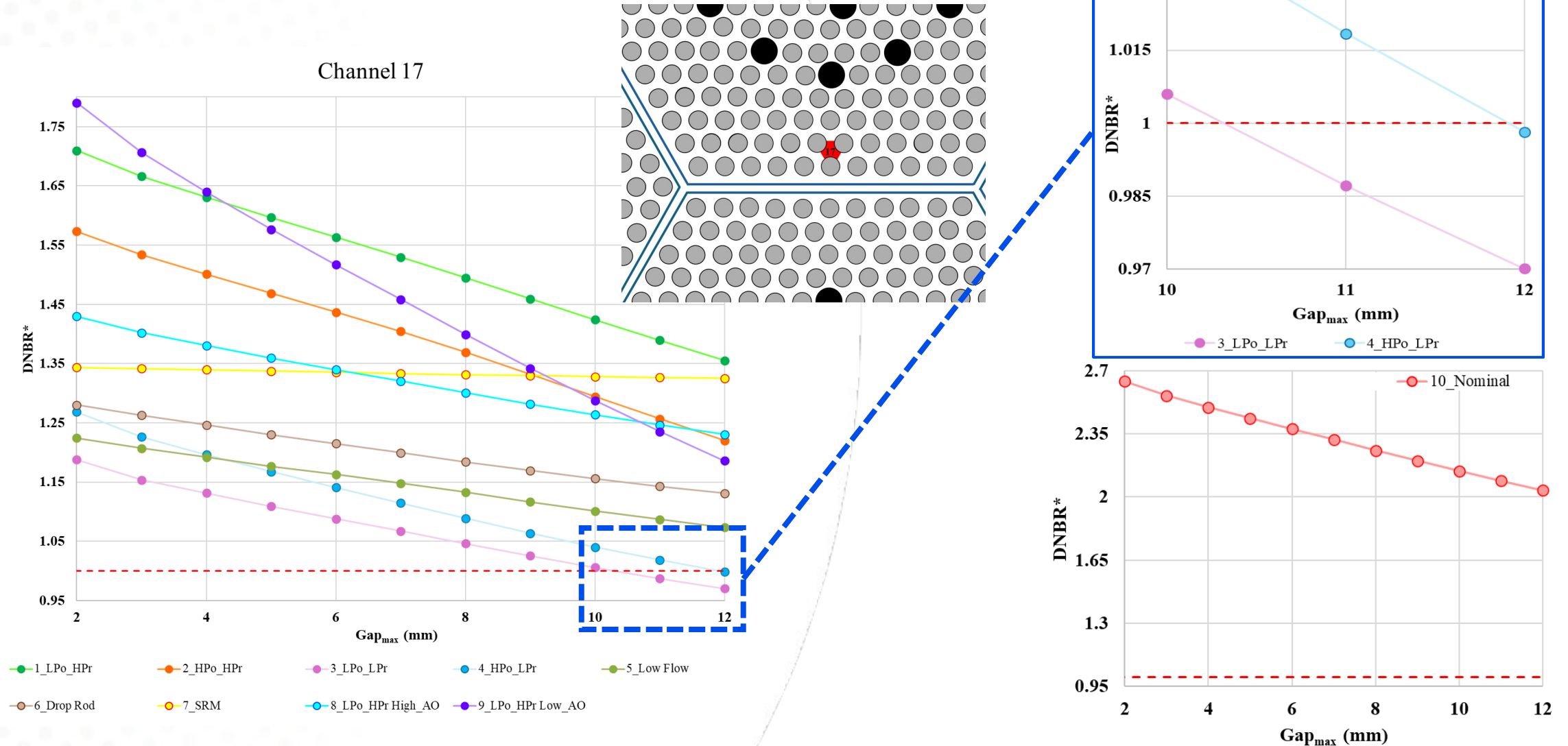


Verification of DL DNBR: Reference cases

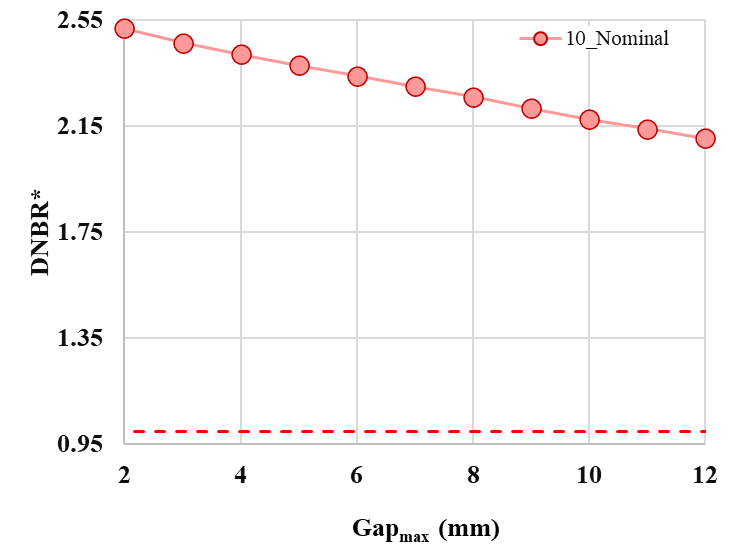
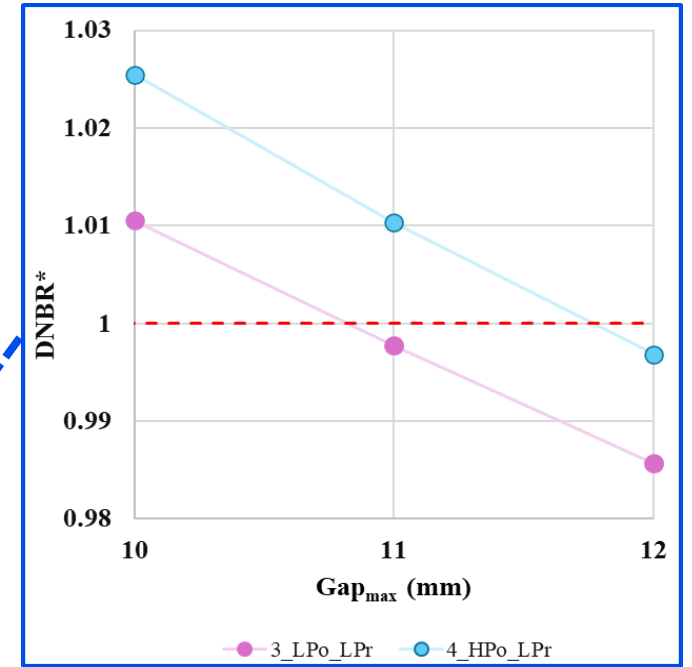
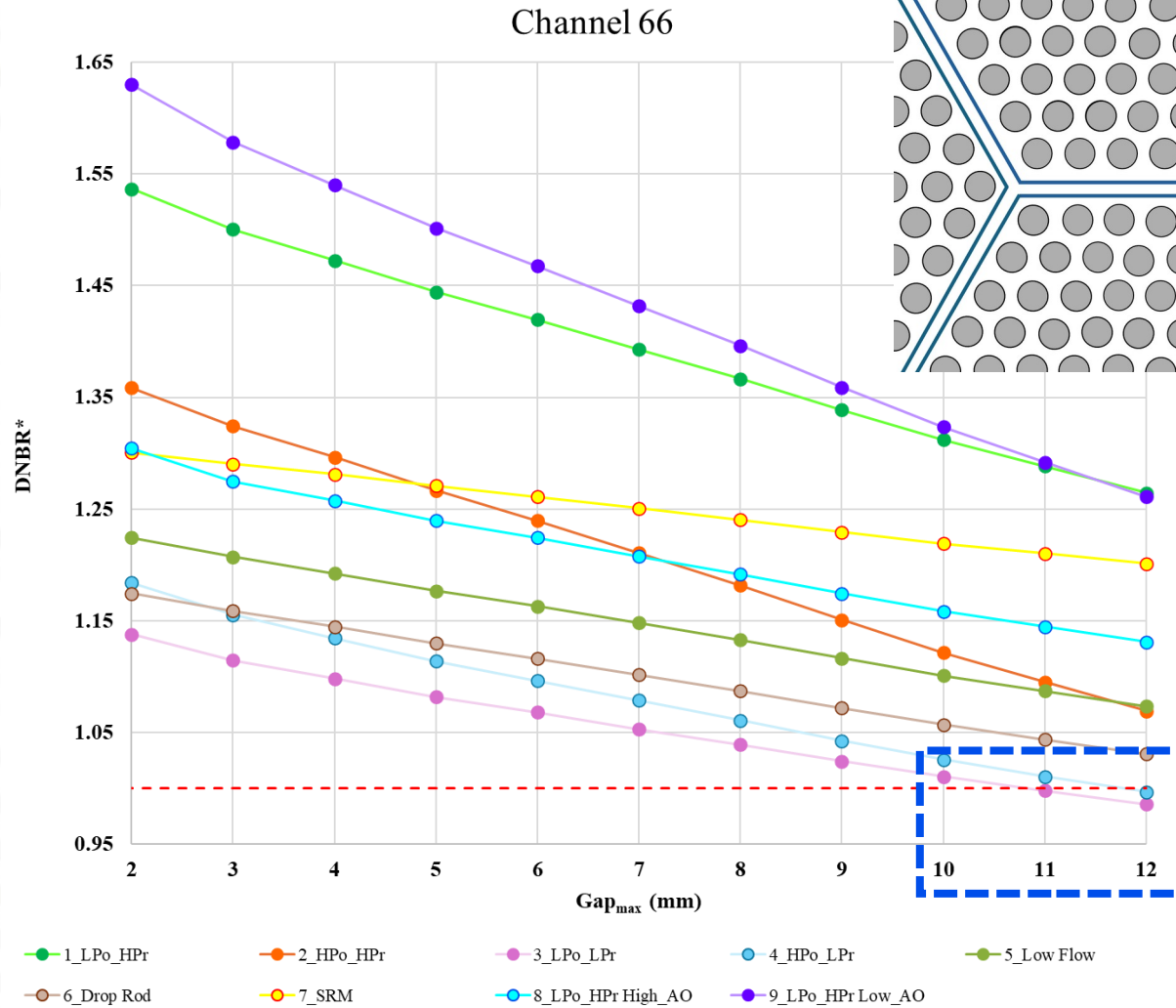


Verification of DL DNBR: Side 1st row

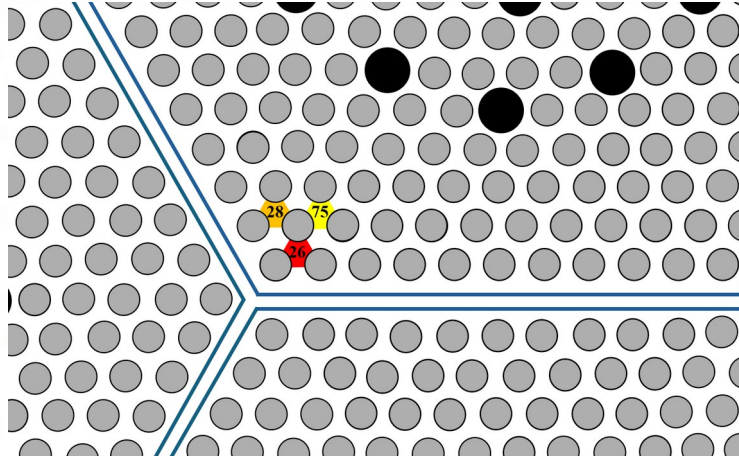
- Introduction of new variable: $DNBR^* = \frac{DNBR_{bow}}{DL\ DNBR}$



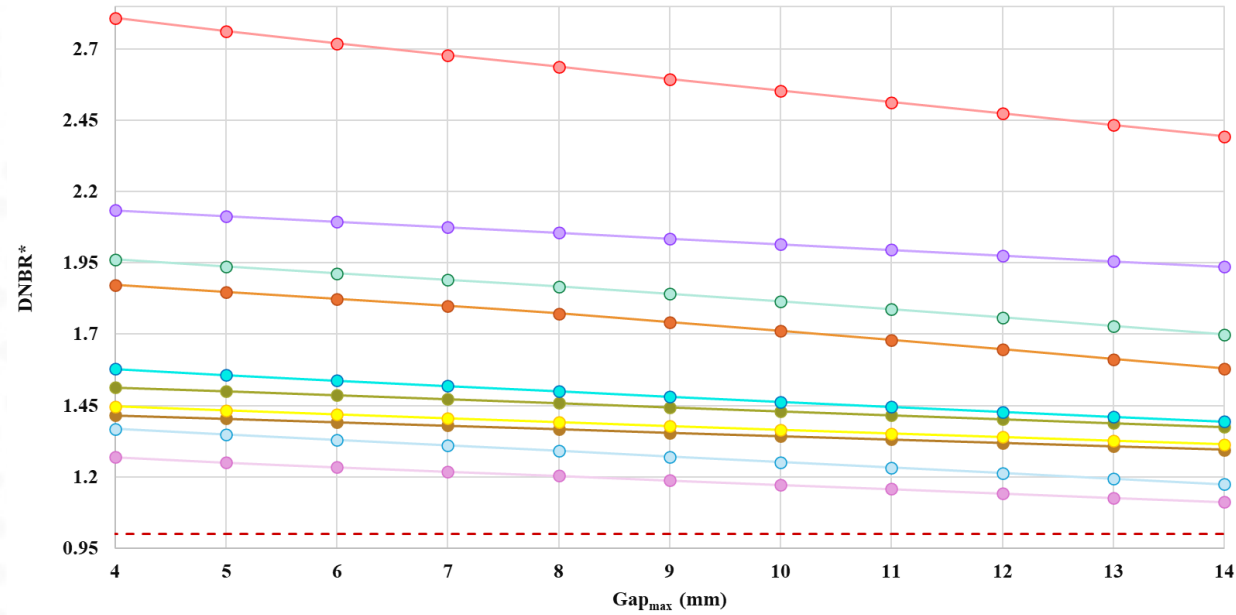
Verification of DL DNBR: Side 2nd row



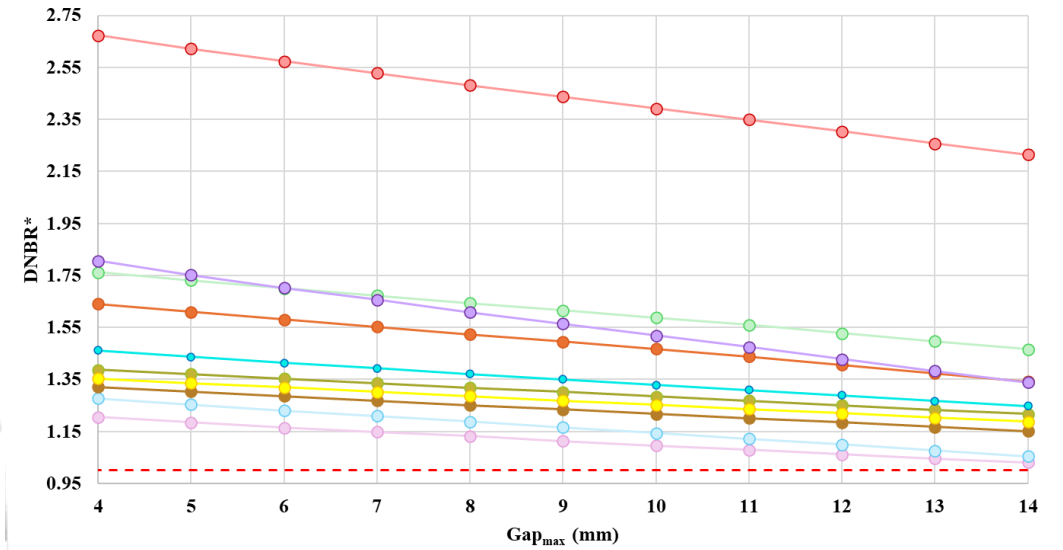
Verification of DL DNBR: Corner



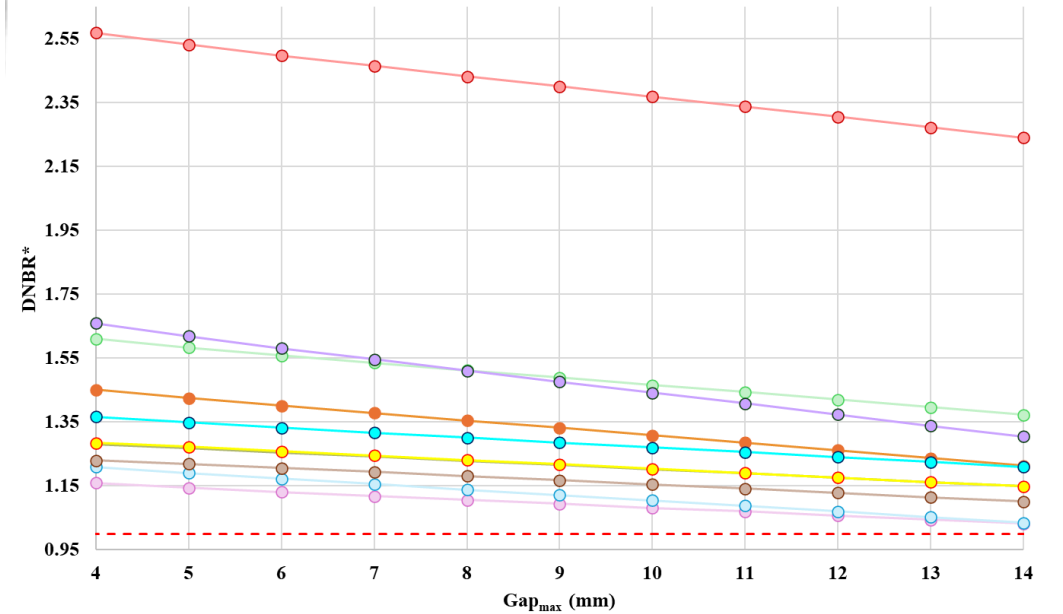
Channel 26



Channel 28



Channel 75



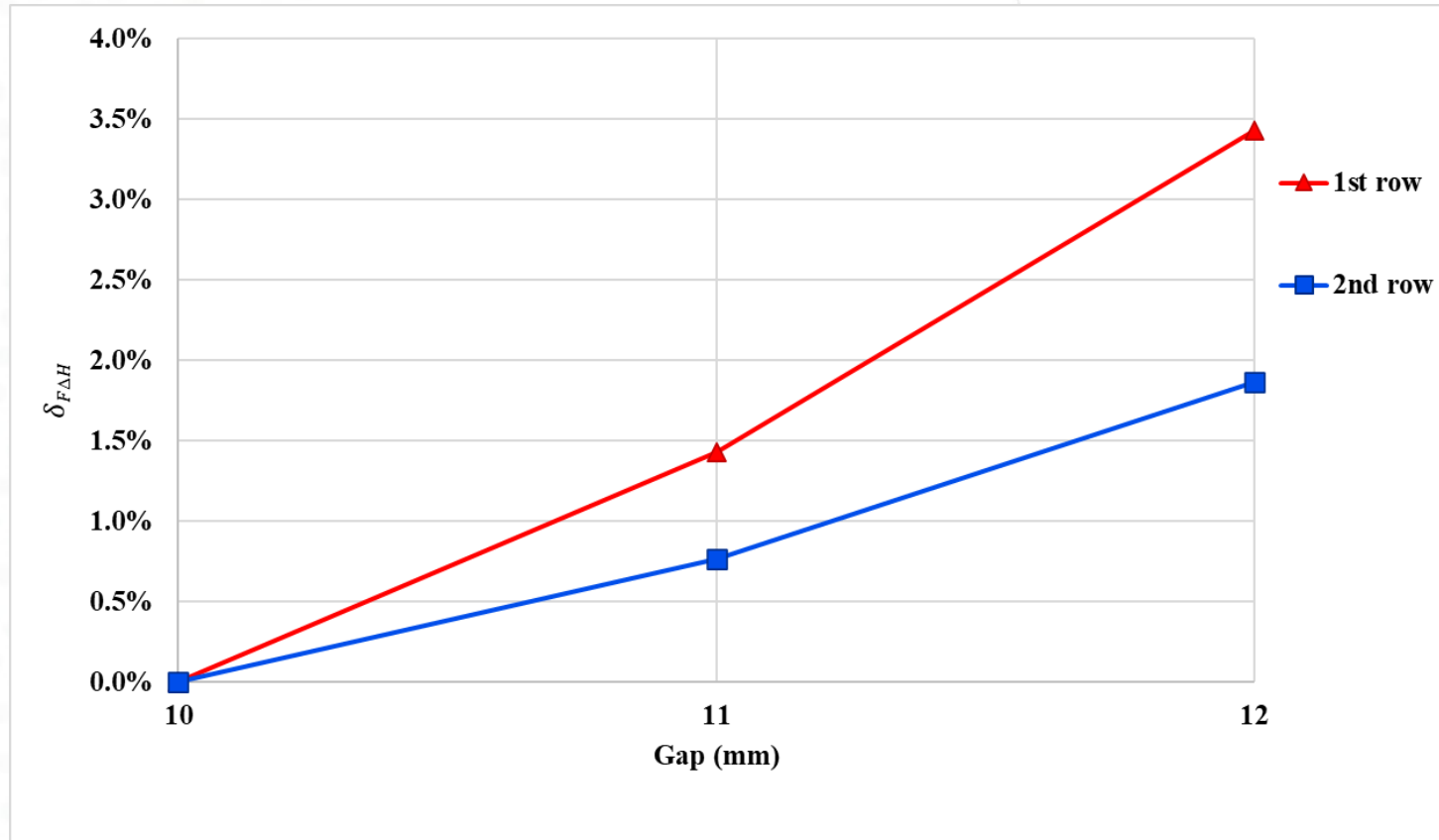
Results



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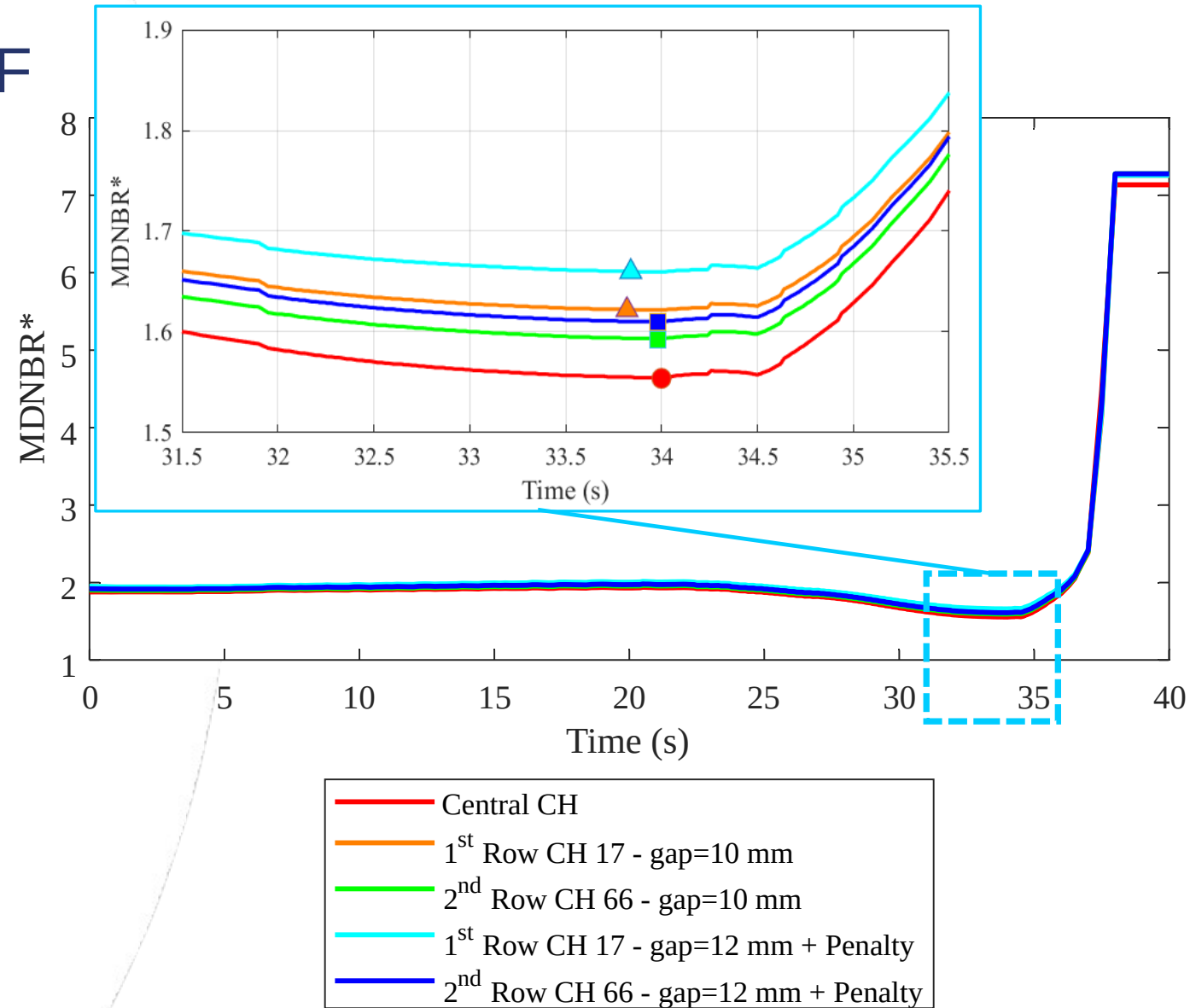
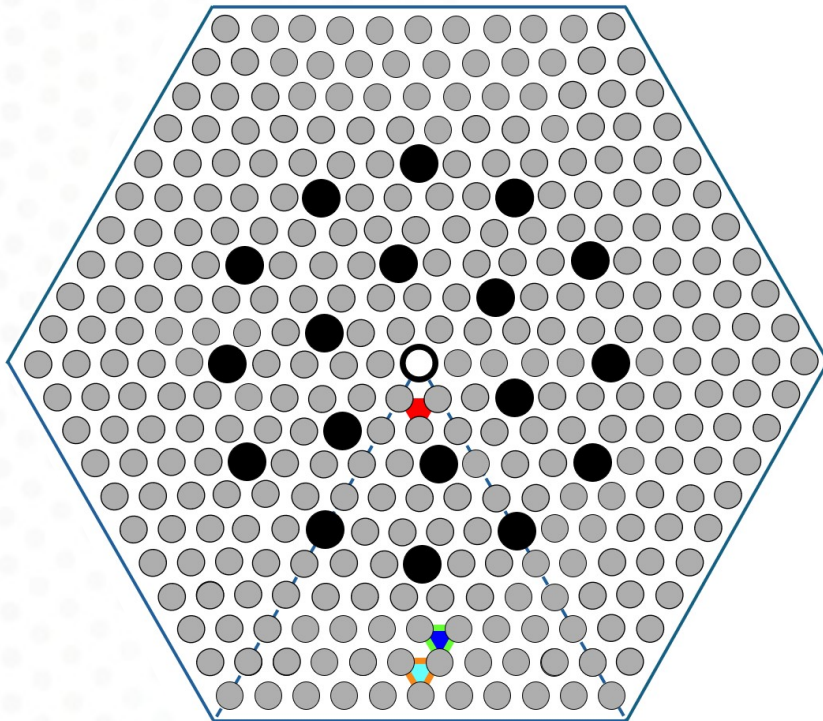
Results: $F_{\Delta H}$ penalty (δ)

- No penalty for gap ≤ 10 mm
- Penalties based on the most conservative values.



Results: Safety analysis verification

- Analysis of CLOF with LONF transient for VVER-1000 shows that hot channel located in interior region remain limiting





Questions?



Thank you